Amendments to the Specification

Please replace paragraph [0057] with a clean version of the following paragraph: [0057] It will be evident from the data of Table 2 that over all of the temperature and time ranges, purges with nitrogen produced only limited and quite unacceptable reductions of the hydrocarbon contamination of the valve. The subsequent purge with the XCDA reduced the hydrocarbon contaminant level to much lower levels, bettering the nitrogen purge lower limit by factors of 225. Further the XCDA purges to the low levels occurred in very short times as compared to the time required for the nitrogen purges to effect significant reductions. (The increases seen for the first nitrogen purge at ambient temperature and the XCDA purge at 80 C between 0 and 60 minutes are believed to be due to the time required for some hydrocarbon contaminants within the elastomeric components to migrate to the surface for purging. This is a physical phenomenon of the elastomeric materials of the valve and not of the purge capabilities of the respective gases.)

Please replace paragraph [0063] with a clean version of the following paragraph:

[0063] Figure 16 is a graph 1600 of time 1602 versus ethylbenzene concentration 1604 for four purge gas mixtures exiting the wafer chamber of Figure 5, the purge gasses containing 100% nitrogen, 20% oxygen, 0.5% water and 100 ppm water according to an embodiment of the present invention. The hydrocarbon-nitrogen contamination mixture was 60 ppb total hydrocarbon concentration, as described in Example 6. Data representing the purge response of ethylbenzene to UHP nitrogen 1608, 20% oxygen (by volume) in

nitrogen 1608 1606, 100 ppm water (by volume) in nitrogen 1610 and 0.5% water (by volume) in nitrogen 1612 are plotted in graph 1600. Purging effectiveness increases as water concentration increases within the ranges of water concentration shown.